

An update of sour performance testing and field performance

Bruce Reichert, PhD

Tenaris Coiled Tubes

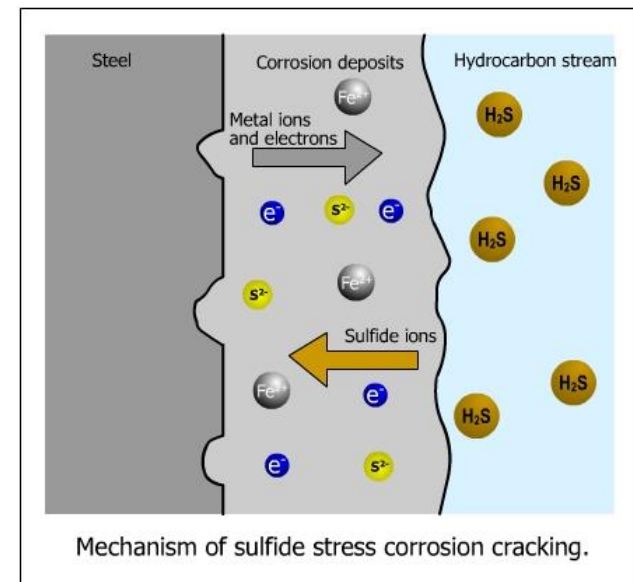
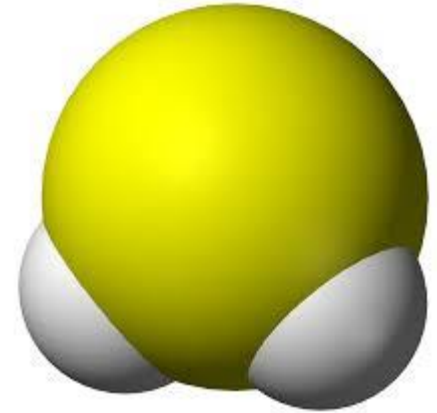


Overview

- Damage Mechanisms
- Industry Standards
- Governing Parameters
- Mitigation Methods
- Testing and Results
- Conclusions

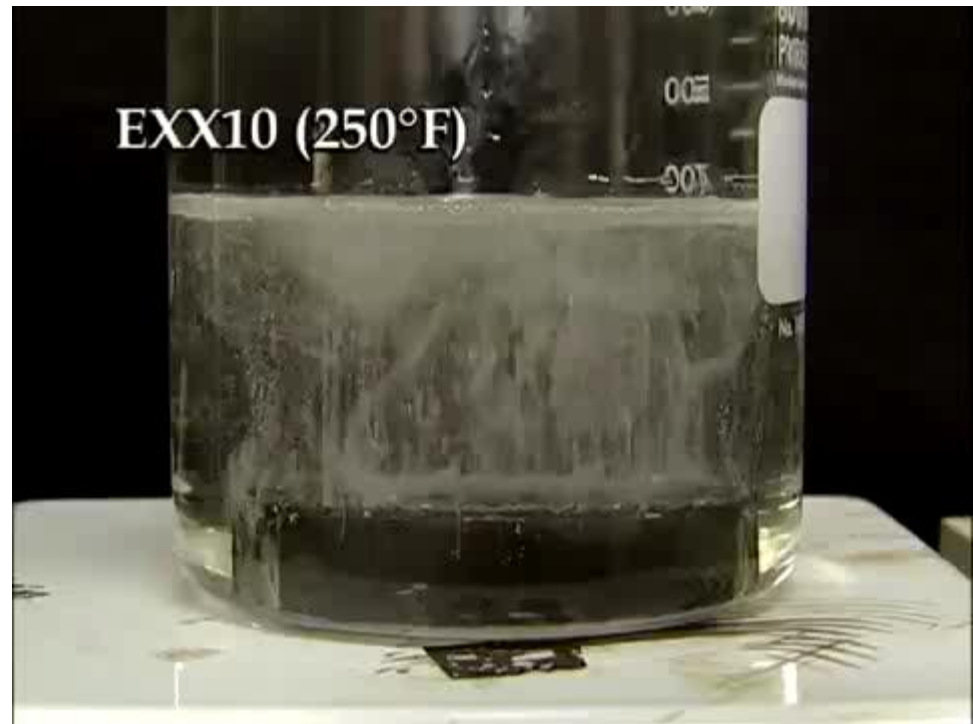
H₂S Corrosion

- Iron becomes anode and H₂S becomes cathode
- $Fe + H_2S + H_2O \rightarrow FeS + 2H + H_2O$
- Normally atomic hydrogen will recombine to molecular hydrogen H_2
- Sulfur restricts recombination of hydrogen



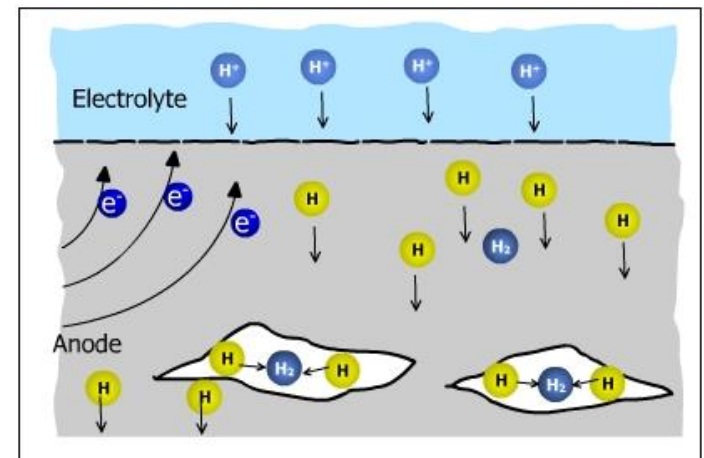
Hydrogen Absorption and Diffusion

- Monatomic hydrogen is absorbed into the steel
- Hydrogen diffuses through steel and concentrates in areas of high stress in the iron lattice (SSC) or weak internal interfaces (HIC)



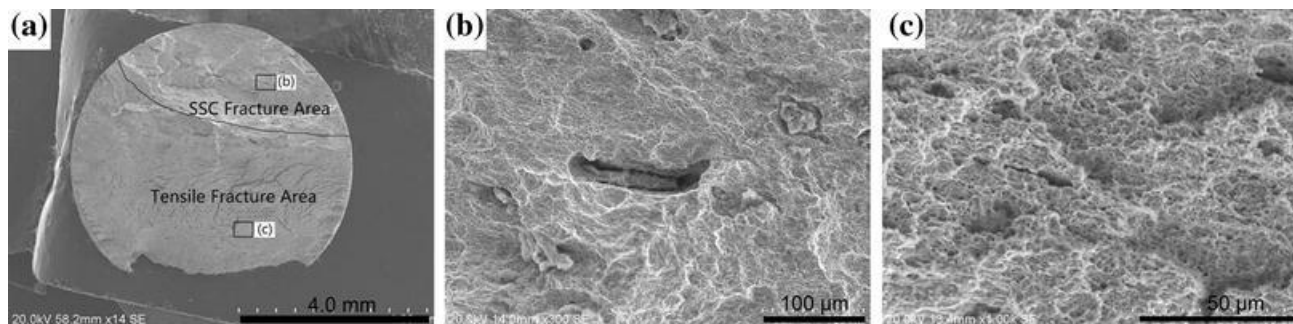
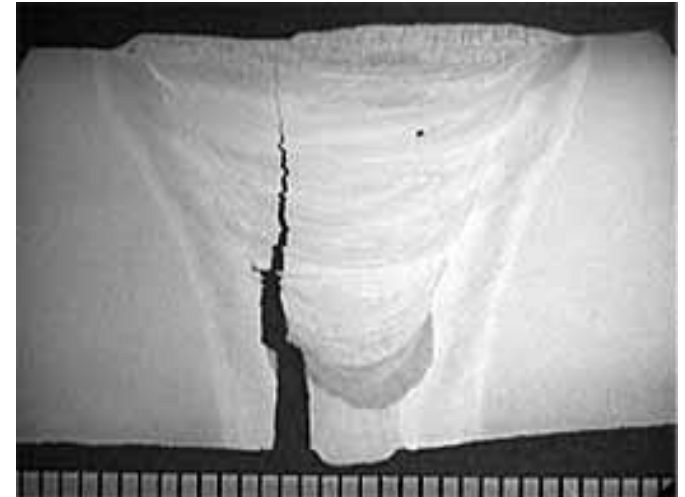
Hydrogen Induced Cracking (HIC)

- Hydrogen recombines at weak internal interfaces (inclusions, laminations, etc.)
- Does not require stress
- Hydrogen recombines into molecular hydrogen
- More common in steels with yield strength <100 ksi
- Steels containing sulfur and phosphorus are more susceptible



Sulfide Stress Cracking

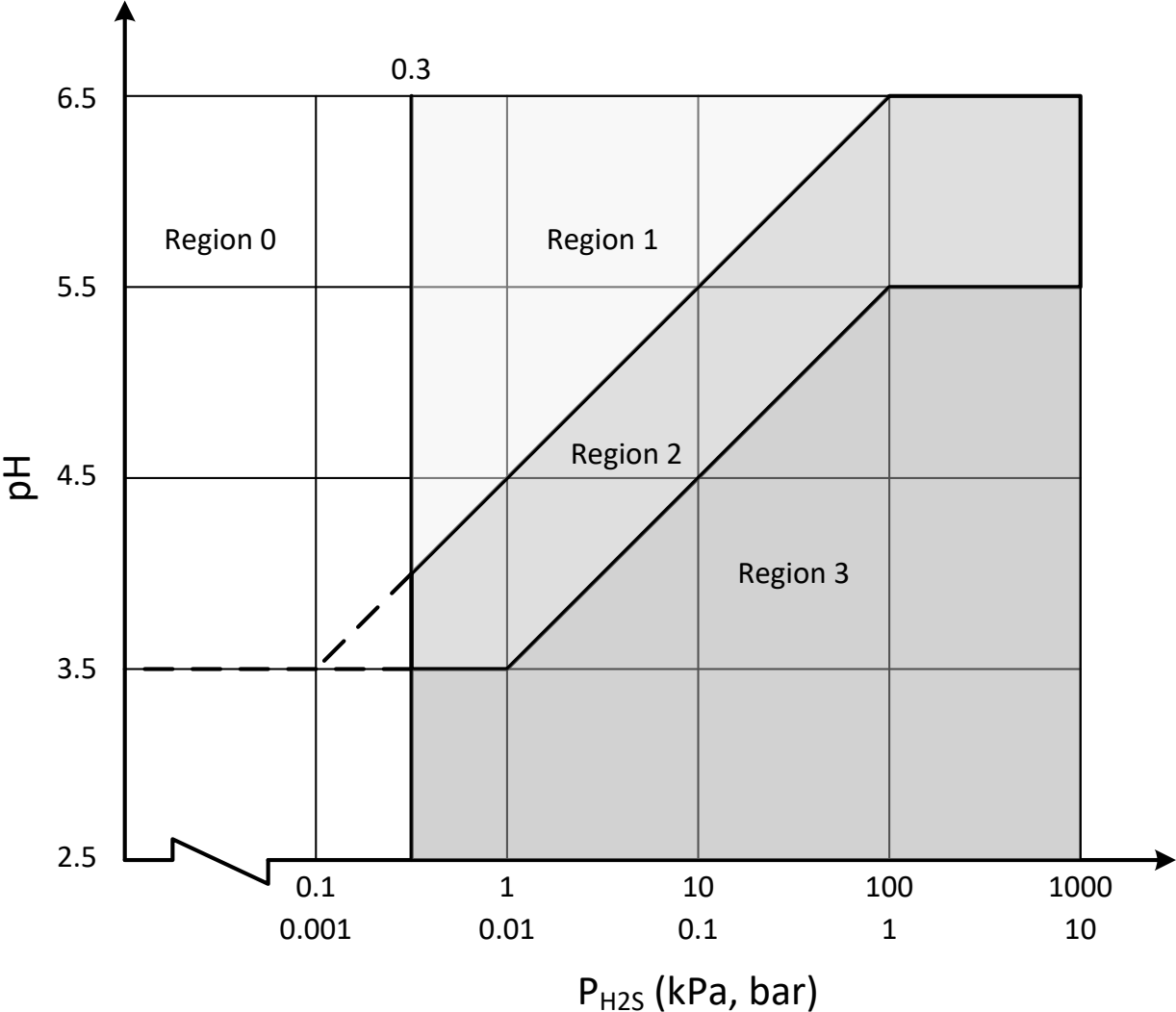
- Monatomic hydrogen remains in iron lattice
- Requires tensile stress
- Produced brittle fracture oriented transverse to stress
- Fractures occur as stress levels below yield
- More common in higher strength steels



NACE MR0175/ISO 15156 – Option 1

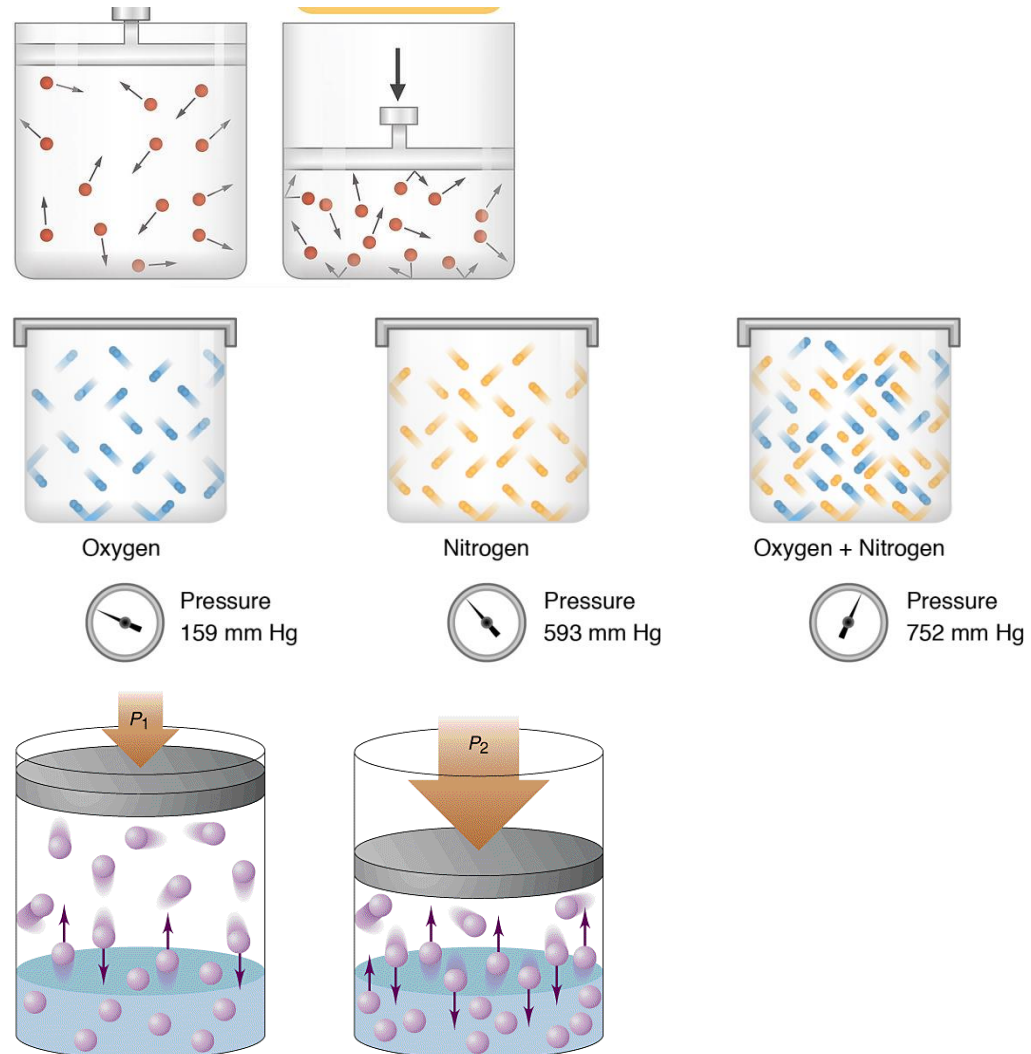
- Doesn't apply to coiled tubing, but
- For $P_{H_2S} < 0.3$ kPa (0.05 psi) “... no special precautions are required ...”
- For $P_{H_2S} \geq 0.3$ kPa (0.05 psi)
 - Heat treatment condition
 - max hardness 22 HRC
 - <1% Ni
 - >1100 F stress relief ($\epsilon > 5\%$)

NACE MR0175/ISO 15156 – Option 2



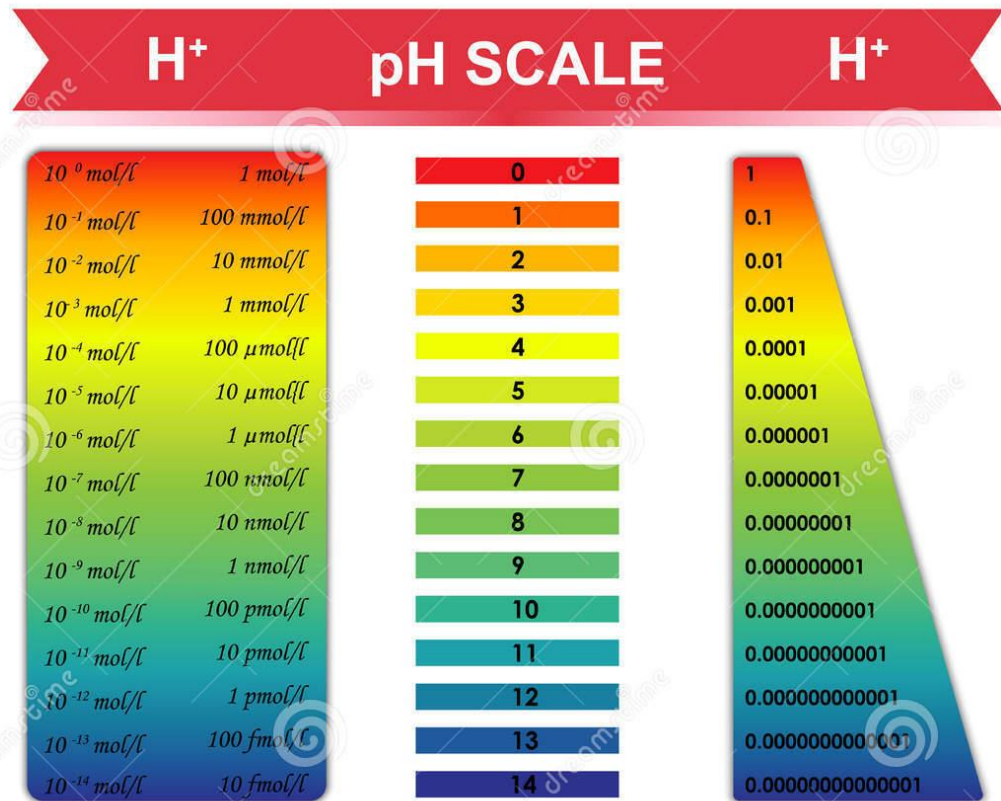
Partial Pressure

- Boyle's law: $PV = C$ The higher the pressure, the more gas molecules per volume
- Dalton's law $\frac{P_i}{P} = \frac{n_i}{n}$ The partial pressure of a gas component is proportional to its concentration
- Henry's law - the amount of dissolved gas is proportional to its partial pressure in the gas phase



pH

- Logarithmic measure of hydrogen ion concentration
- Provides source of monatomic hydrogen if sulfur is present



Download from
Dreamstime.com

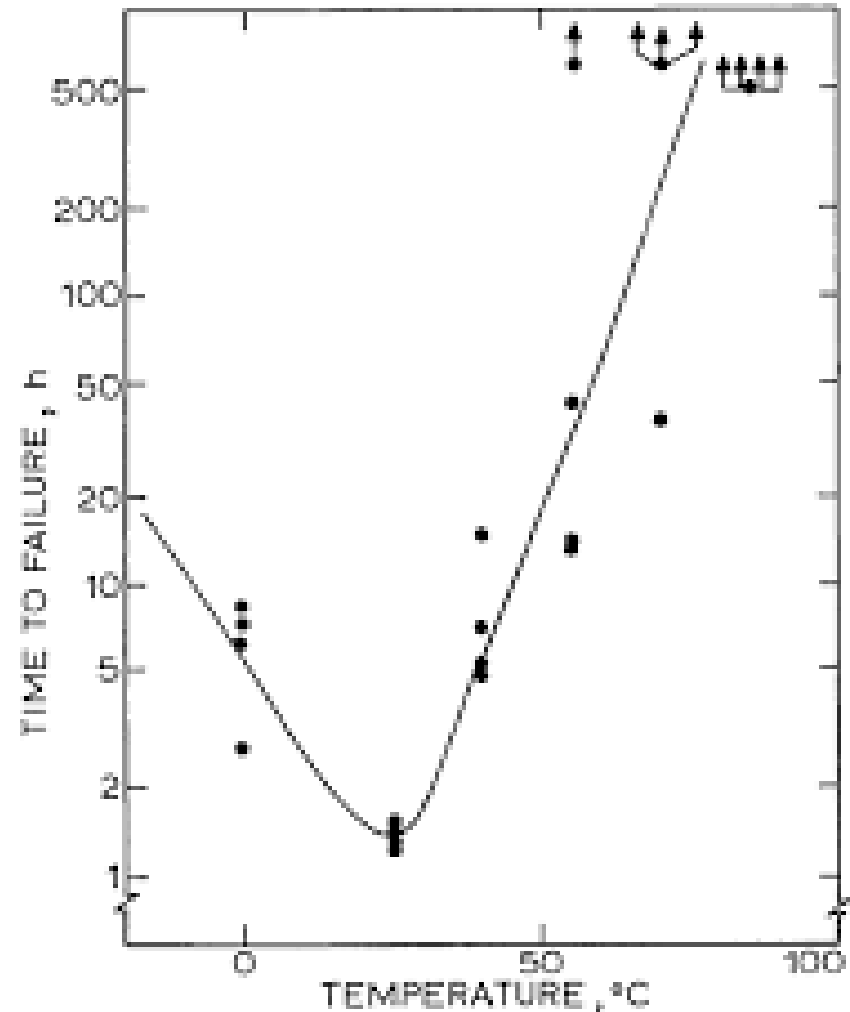
This watermarked comp. image is for previewing purposes only.

ID 56322841

© Extender01 | Dreamstime.com

Temperature

- Maximum susceptibility to SSC and HIC occurs at ambient temperature
- This appears contradictory with the fact that the hydrogen diffusion rate increases with temperature
- At higher temperatures the surface film may be reducing hydrogen adsorption rate

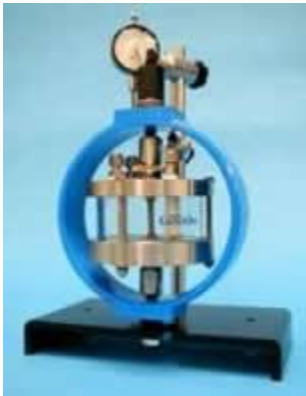


Inhibitors and Scavengers

- Inhibitors have, in general, proven effective in reducing H₂S corrosion, but what about SSC and HIC?
- Inhibitors are typically fatty amine based and attach to the FeS film layer on the tube surface
- Surface film becomes hydrophobic, significantly decreasing water activity and hydrogen ion concentration
- Scavengers can reduce H₂S concentration

SSC Testing and Results

NACE TM0177



Method A
UT



Method B
FPB



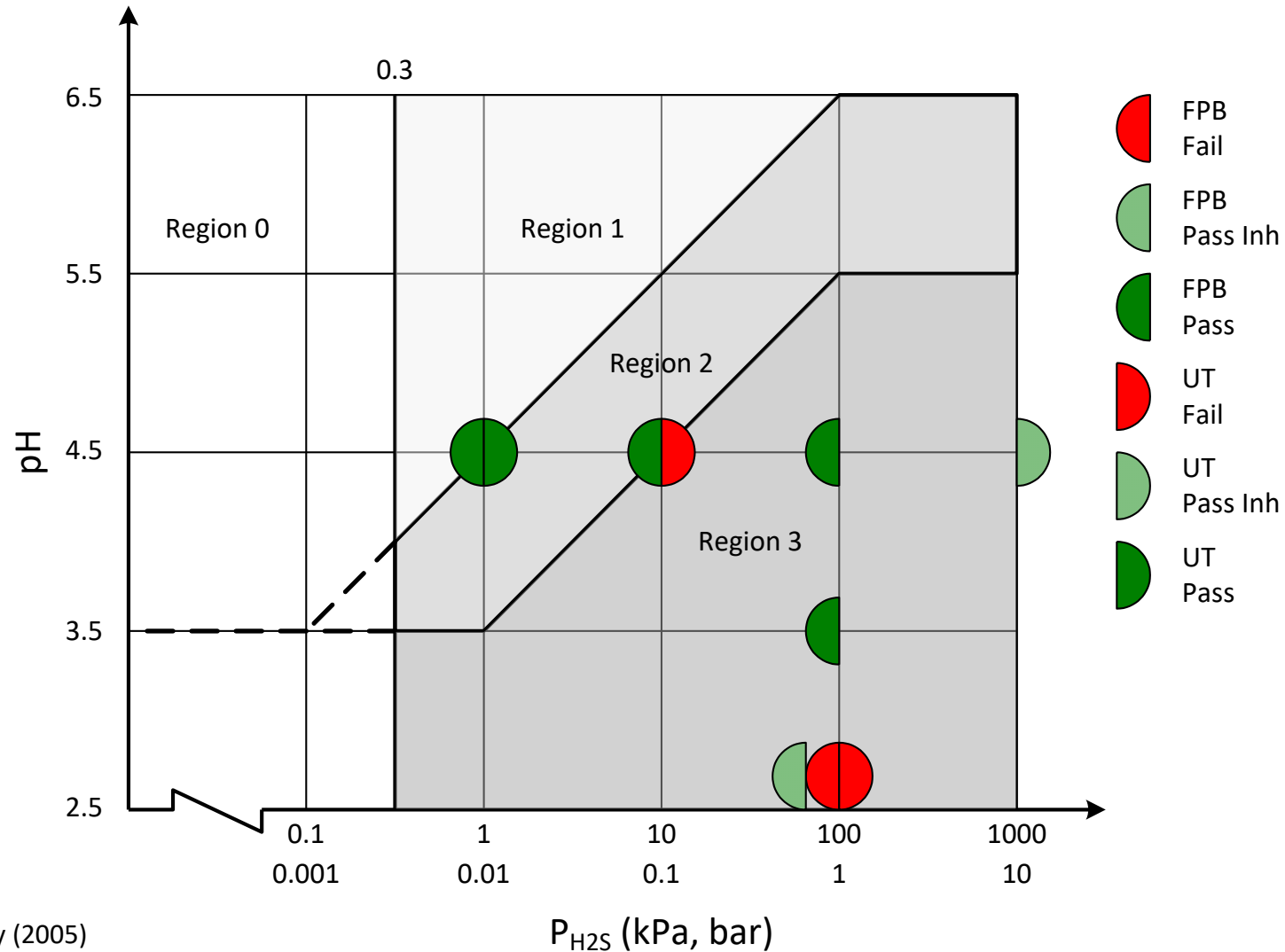
Method C
CR



Method D
DCB

- Applied stress (usually % of SMYS or AYS)
- 30 day duration
- Typically ambient temperature and pressure
- Solution A – pH 2.6 to 2.8, 1 bar H₂S
- Solution B - pH 3.4 to 3.6, 1 bar H₂S

SSC Testing With and Without Inhibitor



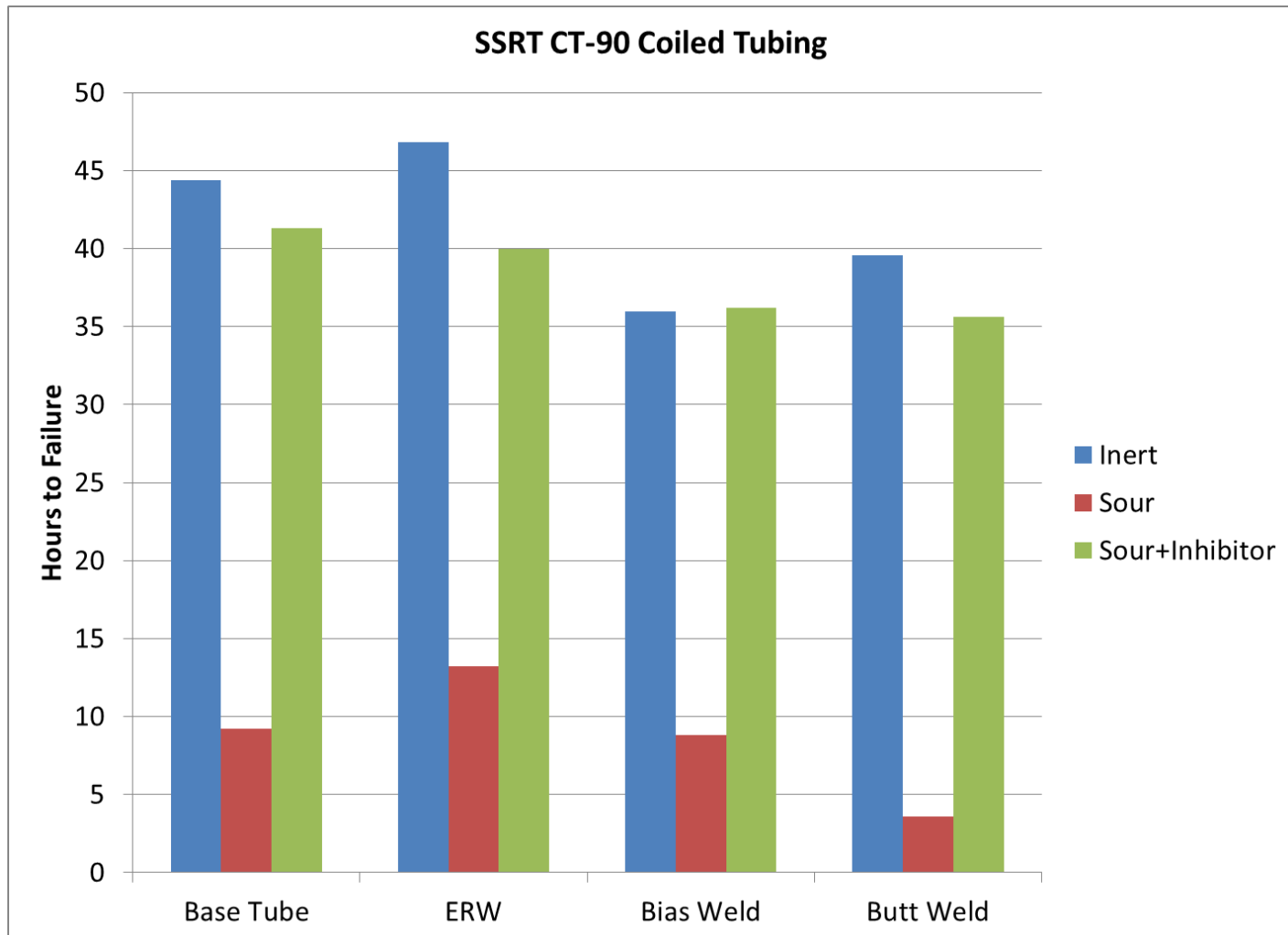
SSR Testing and Results

Slow Strain Rate Testing (SSRT)

- Strain rate of 1×10^{-6}
- Strain continues to failure
- Compare time to failure in inert and sour environments

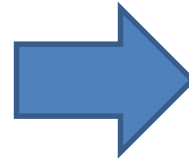


SSRT With and Without Inhibitor

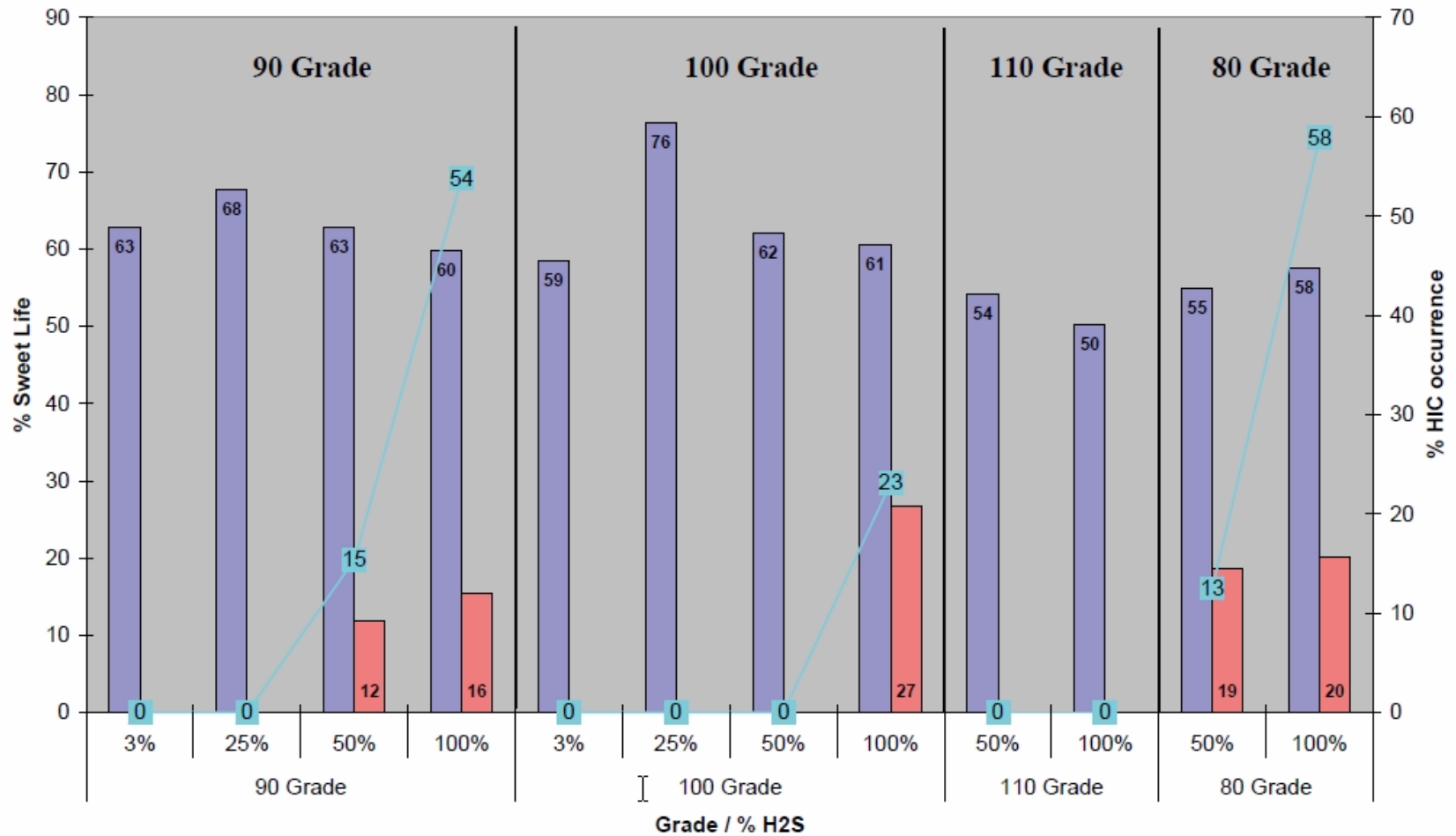


Sour Fatigue Testing and Results

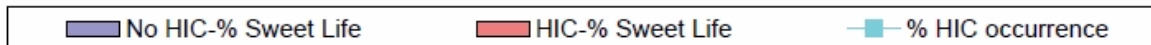
- Full size bend fatigue samples are exposed in sour environment for 4 to 7 days
- Samples are transported on dry ice to bend fatigue machine
- Samples are repeatedly bent at straightened with internal pressure until fracture occurs
- Comparison made of fatigue life with and without sour exposure



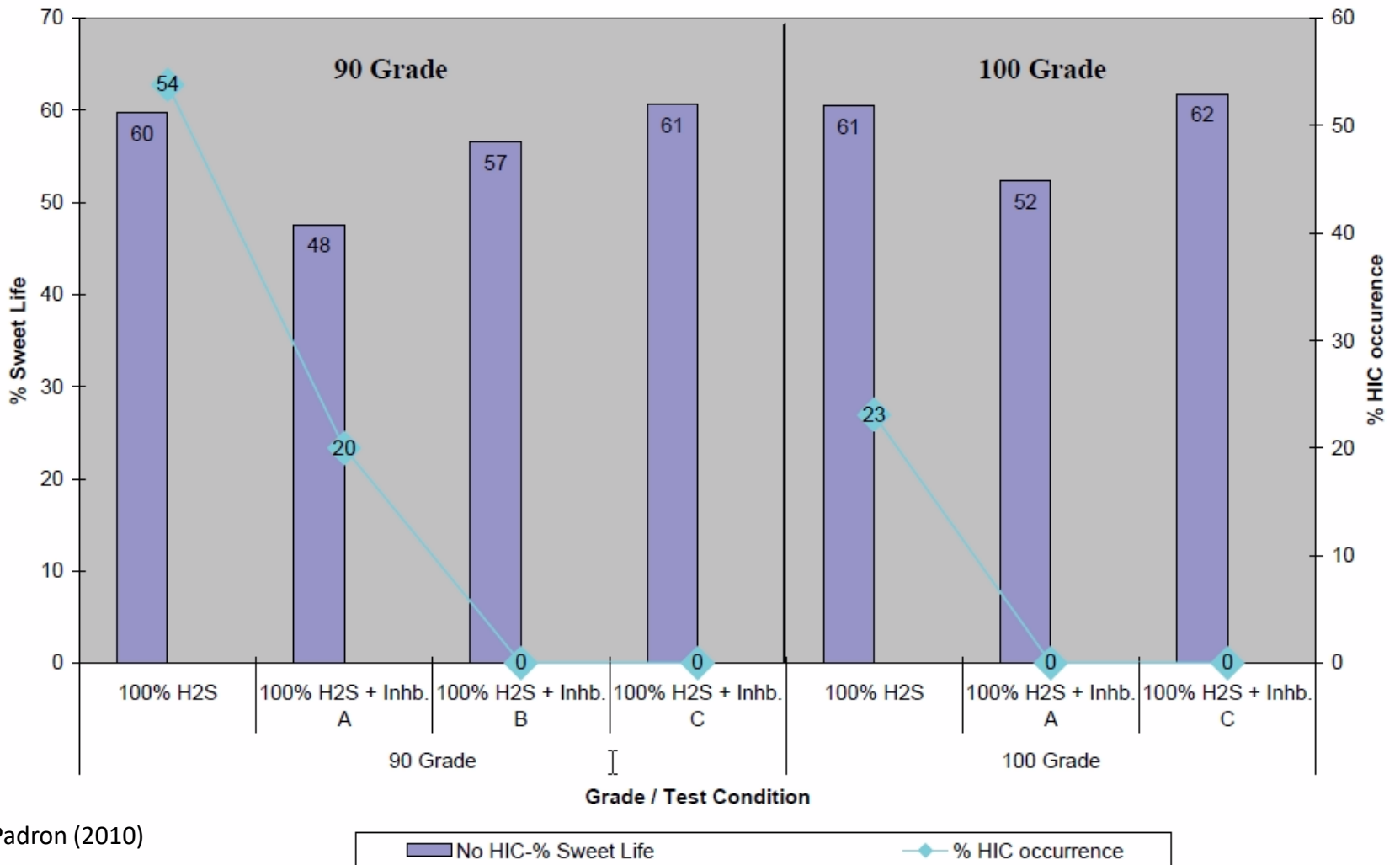
Base Tube Sour Fatigue Without Inhibitor



Source: Padron (2010)

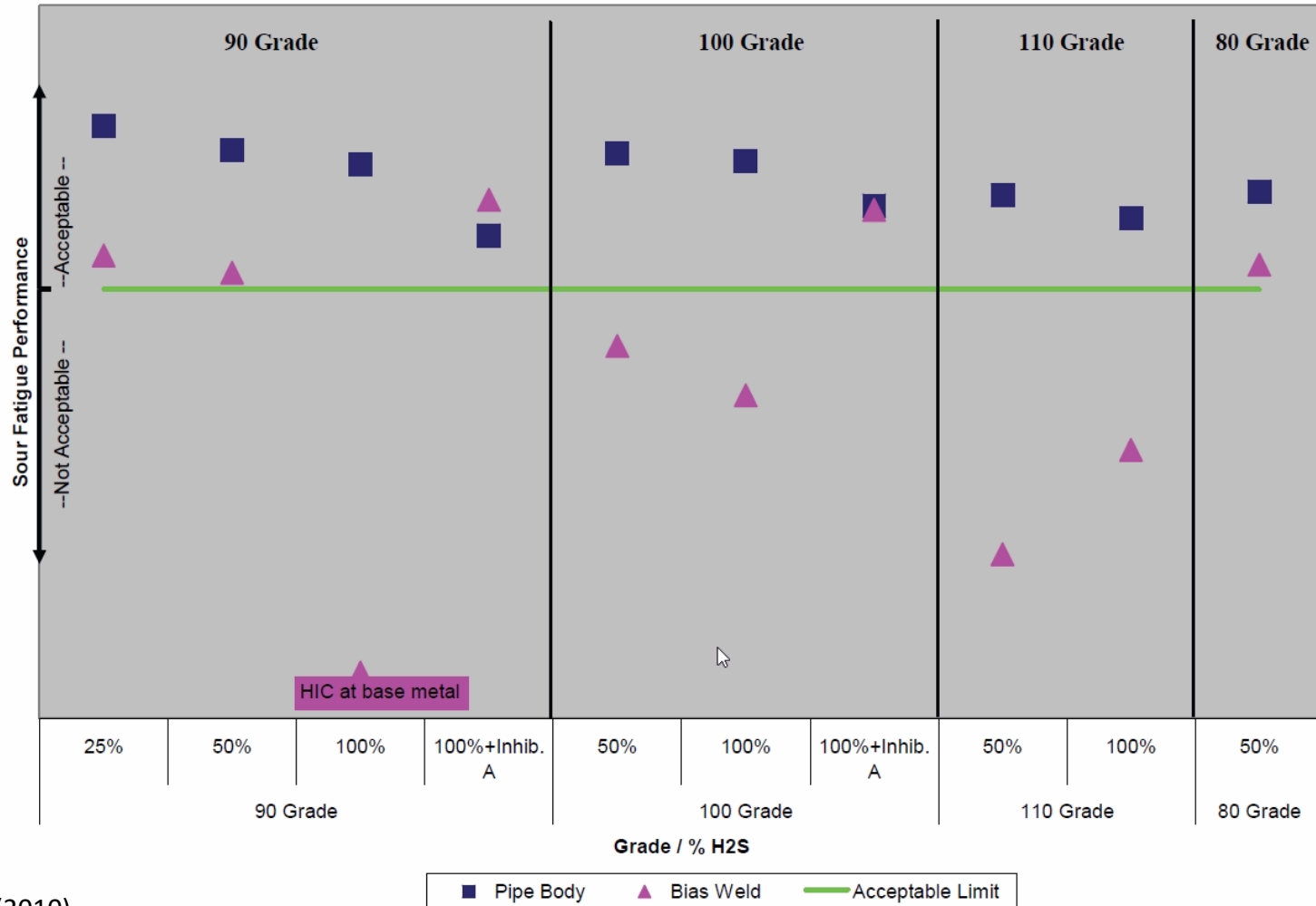


Base Tube Sour Fatigue With Inhibitor



Source: Padron (2010)

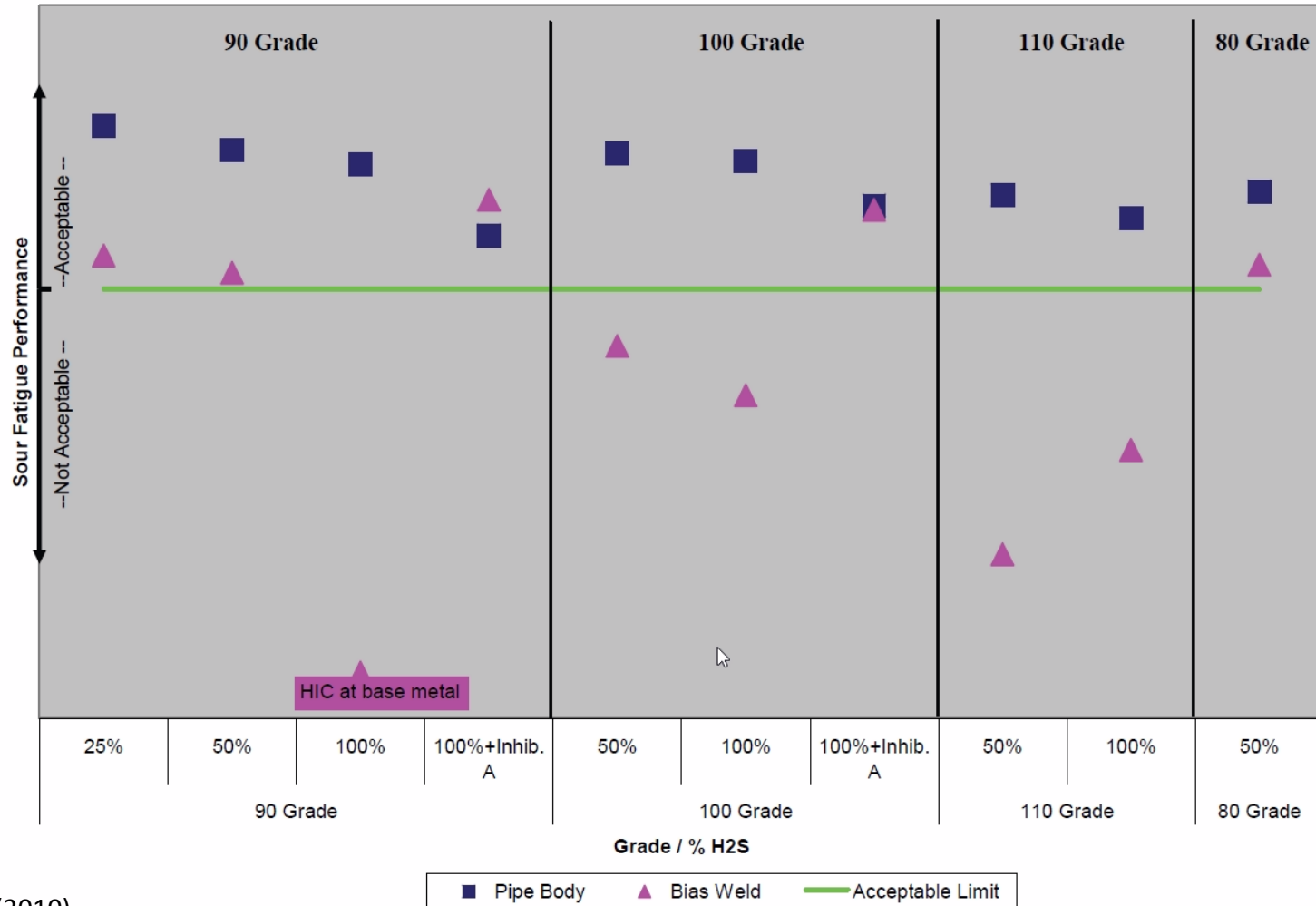
Bias Weld Sour Fatigue Without Inhibitor



Source: Padron (2010)

Figure 13. Bias welds sour fatigue performance

Bias Weld Sour Fatigue Without Inhibitor

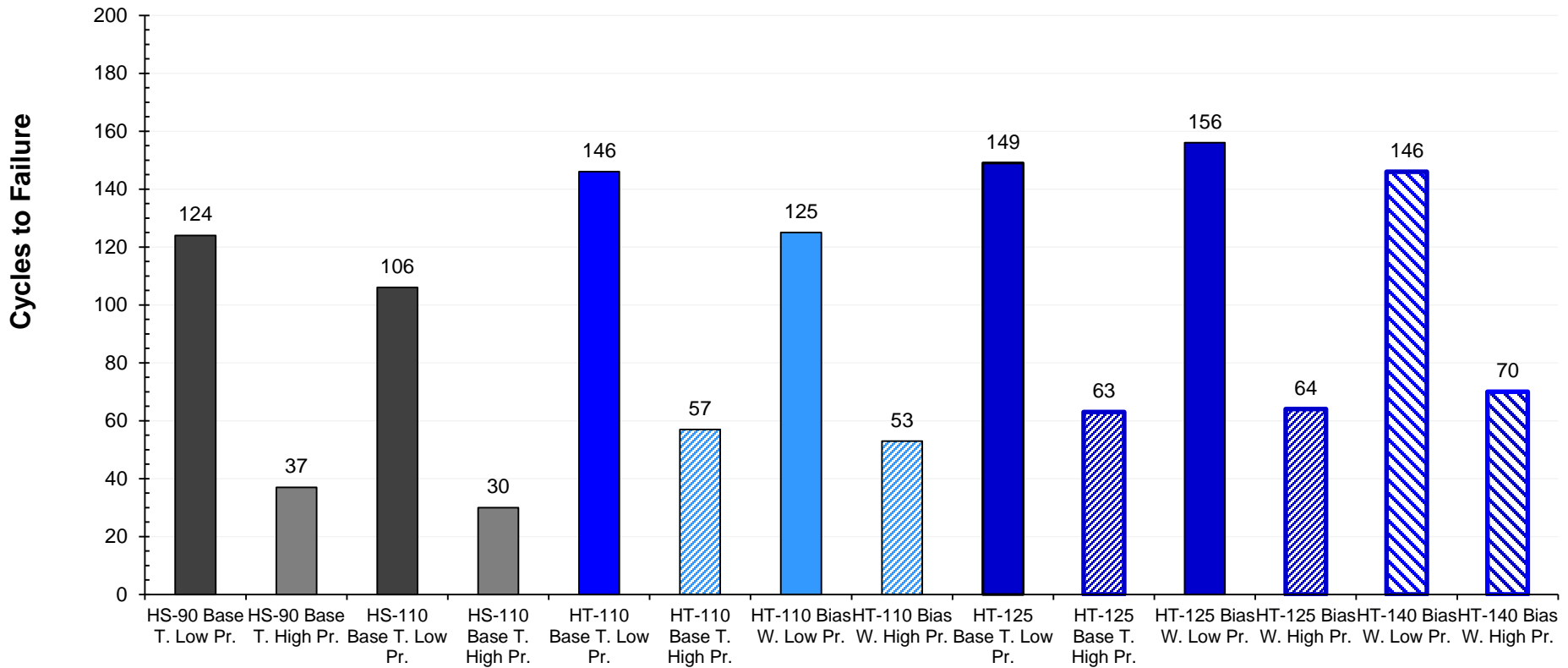


Source: Padron (2010)

Figure 13. Bias welds sour fatigue performance

BlueCoil Sour Fatigue Life Without Inhibitor

Sour Fatigue Results



Conclusions

- Time to SSC failure in sour environments were typically <10 hours
- Inhibitors proved effective at reducing susceptibility to SSC
- Cumulative fatigue prior to testing did not significantly increase susceptibility to SSC
- Ignoring HIC failures, the sour fatigue life was essentially constant (50%-60%) and independent of grade and H₂S partial pressure (within the range tested)
- HIC will significantly reduce sour fatigue life
- HIC failures increased with H₂S partial pressure and decreased with increasing tube SMYS
- Inhibition does not extend sour fatigue life, except for avoiding HIC
- Bias weld sour fatigue life is significantly lower than base tube sour fatigue life

References

- H. E. Townsend, Jr., “Hydrogen Sulfide Stress Corrosion Cracking of High Strength Steel Wire,” Corrosion Vol. 28, No. 2, pp. 39-46, (1972)
- T. McCoy, “SSC Resistance of QT-900 Coiled Tubing,” paper SPE 93786, SPE/ICoTA Coiled Tubing Conference and Exhibition, The Woodlands, Texas, April 12-13, (2005)
- T. Padron, “Sour Serviceability of Higher-Strength Coiled Tubing: Final Results,” paper SPE 130279, SPE/ICoTA Coiled Tubing and Well Intervention Conference and Exhibition, The Woodlands, Texas, March 23-24, (2010)
- R. Hampson, C. Moir and T. Freeney, “Working With Coiled Tubing in H₂S and CO₂ Wells: A Global Perspective,” paper SPE 121294, SPE/ICoTA Coiled Tubing and Well Intervention Conference and Exhibition, The Woodlands, Texas, March 31-April 1, (2009)
- R. D. Kane and M. S. Cayard, “Roles of H₂S in the Behavior of Engineering Alloys: A Review of Literature and Experience,” paper NACE 274, Corrosion 98 (1998)
- “Petroleum and Natural Gas Industries, Materials for use in H₂S-environments in Oil and Gas Production,” NACE International Standard MR0175, ISO 15156, 1st Edition (2003)
- M. Valdez, C. Morales, C., R. Rolovic, R. and B. Reichert, B., “The Development of High-Strength Coiled Tubing with Improved Fatigue Performance and H₂S Resistance,” paper SPE 173639, SPE/ICoTA Coiled Tubing and Well Intervention Conference and Exhibition, The Woodlands, Texas, March 24-25, (2015)